

Recent Developments in SCALE

Presented to:

Nuclear Criticality Safety Program Technical Program Review

Bradley T. Rearden, PhD

Leader, Modeling and Simulation Integration
Manager, SCALE Code System
Reactor and Nuclear Systems Division

March 27, 2018

ORNL is managed by UT-Battelle
for the US Department of Energy

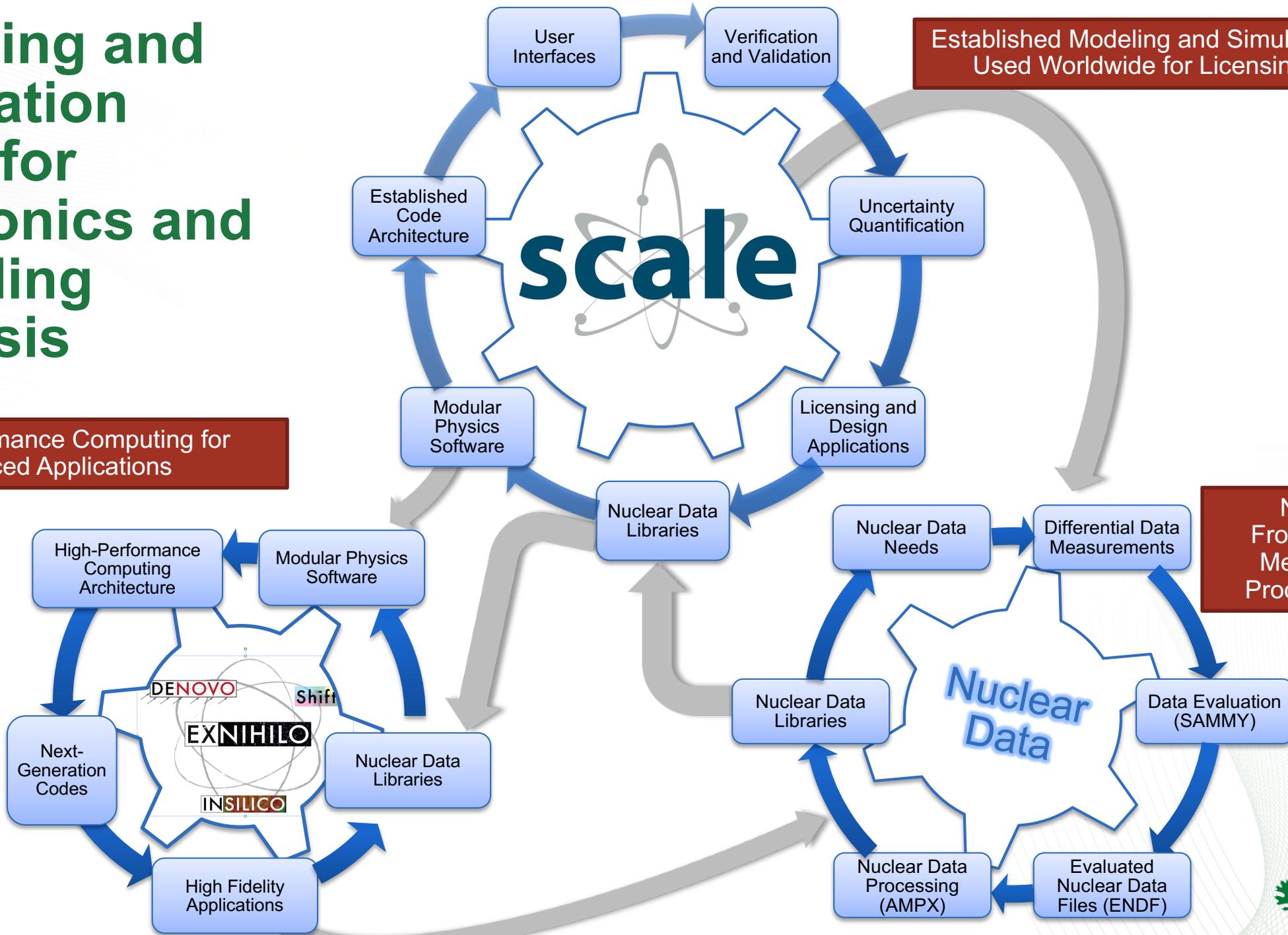


Modeling and Simulation Tools for Neutronics and Shielding Analysis

High-Performance Computing for Advanced Applications

Established Modeling and Simulation Capabilities Used Worldwide for Licensing and Design

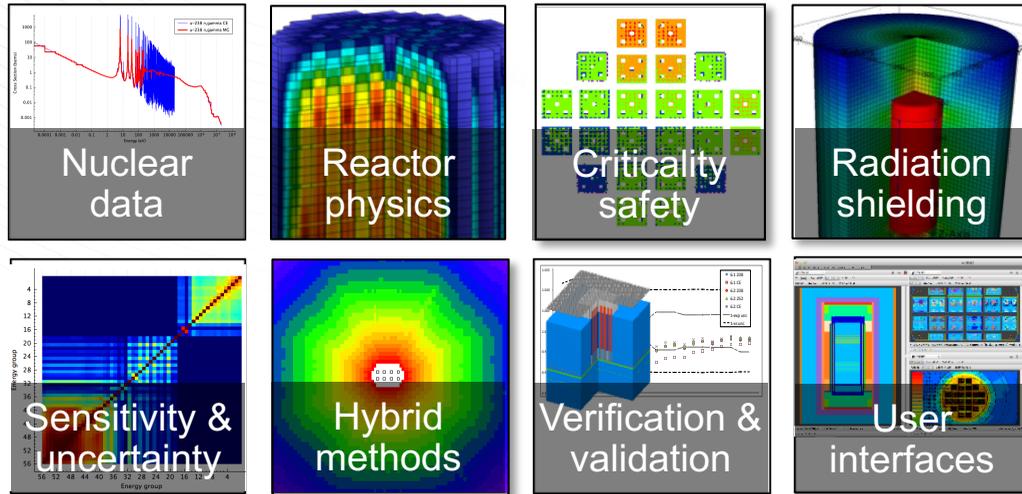
Nuclear Data: From Fundamental Measurements to Production Libraries



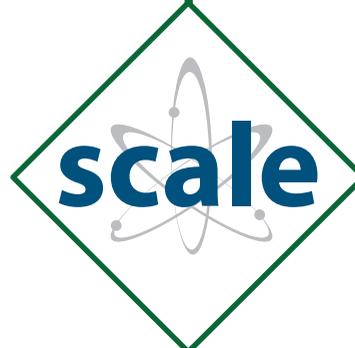
SCALE Code System:

Neutronics and Shielding Analysis Enabling Nuclear Technology Advancements – <http://scale.ornl.gov>

Practical tools relied upon for design, operations and regulation



Global distribution: 8,500 users in 58 nations

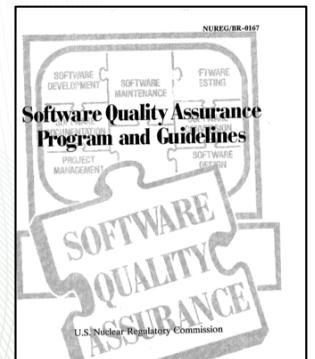
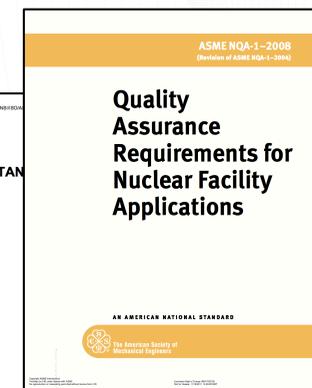
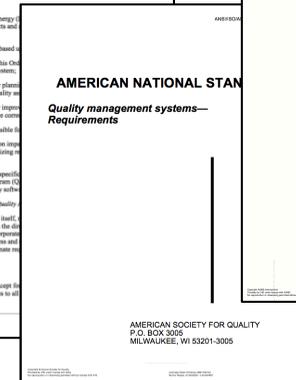
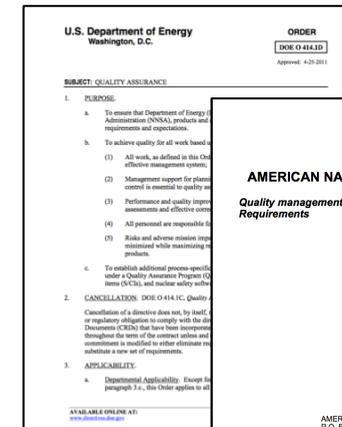


Professional training for practicing engineers and regulators



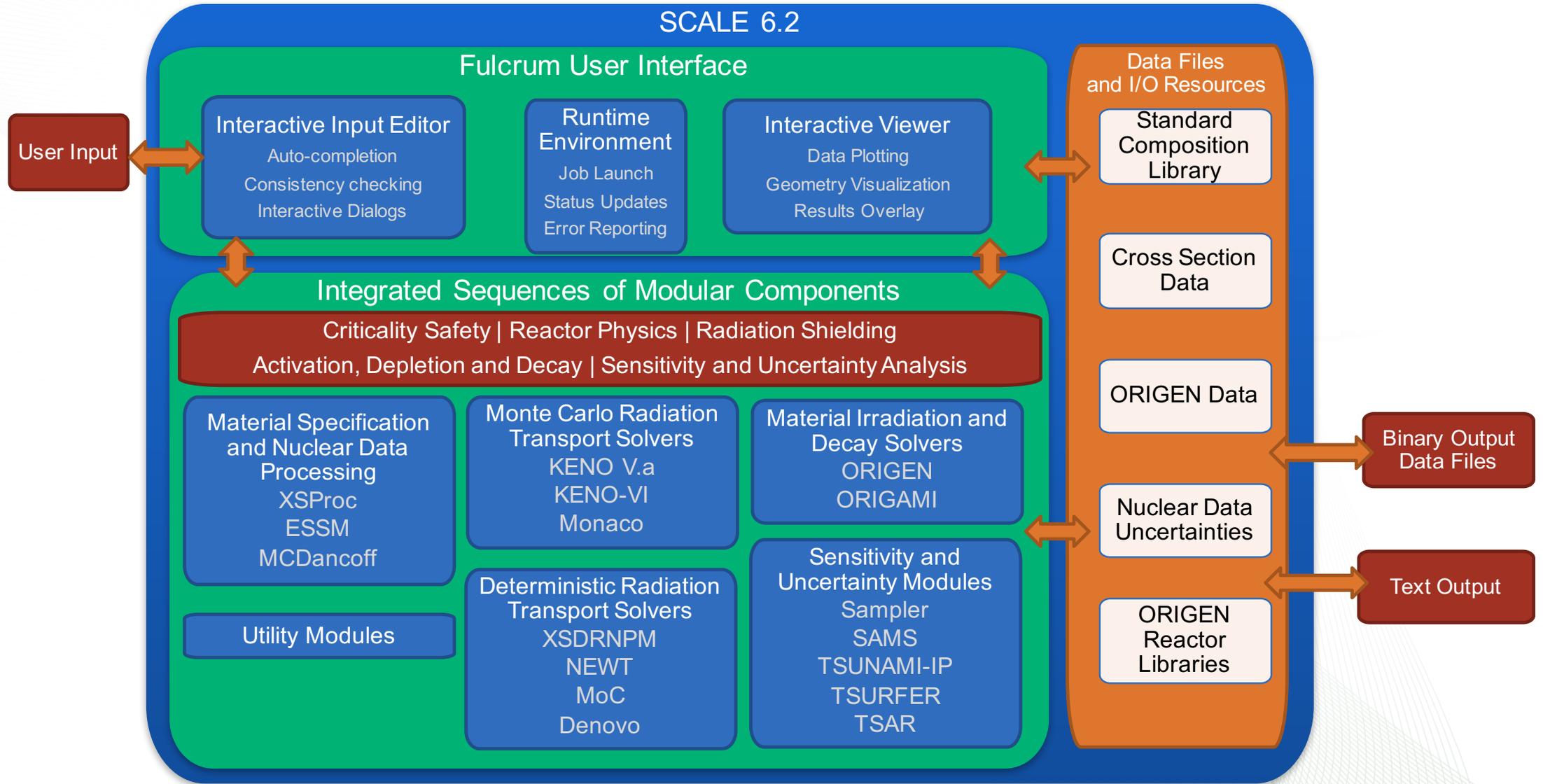
FY17 statistics:
 9 week-long courses
 1 conference tutorial
 110 participants from 14 nations

Robust quality assurance program based on multiple standards

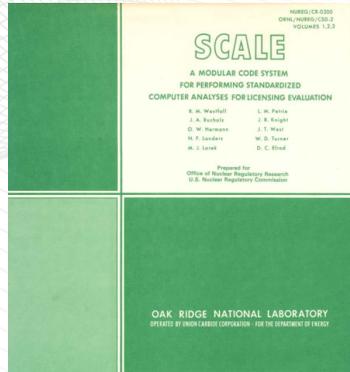


SCALE is an Integrated System with Many Features

- Innovative
- Efficient
- Accurate
- Easy to Use



SCALE Evolution



SCALE 0.0 – SCALE 4.4a

1980 – 2000

Established for Nuclear Regulatory Commission

Provides an independent rigorous nuclear safety analysis capability for out-of-reactor license reviews

Key Capabilities

- Criticality safety
- Radiation source term characterization
- Radiation shielding
- Heat transfer

SCALE 5.0 – SCALE 6.1

2004 – 2011

Expanded Capabilities to Address a Broader Class of Problems & Sponsors

- Reactor physics
 - Shielding analysis with automated variance reduction
 - Sensitivity and uncertainty analysis
 - High-fidelity criticality safety in continuous energy
 - Graphical user interfaces and visualization tools
- ### Expanded visibility
- Used in 56 nations by regulators, industry, utilities, and researchers

SCALE 6.2

2016 – 2018

Increased Fidelity, Infrastructure Modernization, Parallelization, Enhanced Quality Assurance

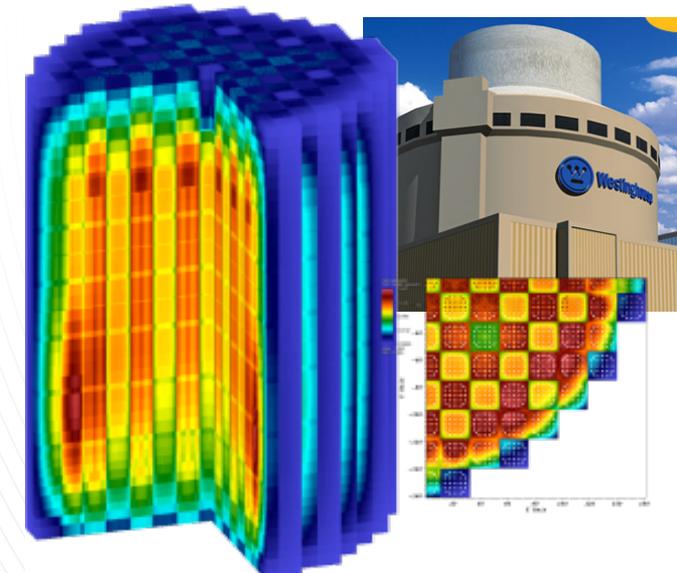
- Solutions for extremely complex systems
 - High-fidelity shielding, depletion and sensitivity analysis in continuous energy
 - Simplified and efficient lattice physics
 - Unified user interface
 - Initiated modern, modular software design
- ### Expanded Use
- Over 8,500 users in 58 nations
Tools leveraged by many projects

SCALE 6.3 – SCALE 7.0

2018 –

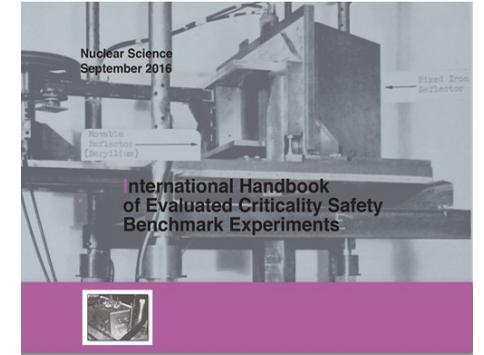
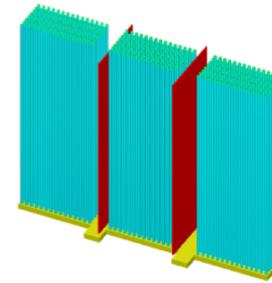
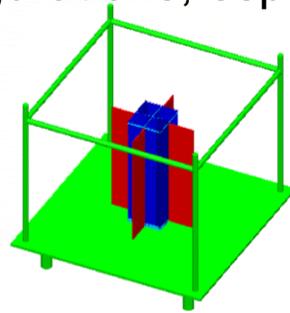
High-performance Monte Carlo, Capabilities for Advanced Reactors and Advanced Fuels, Integration with Many other Tools

- Solutions for extremely complex systems
 - High-fidelity, highly parallelized criticality shielding, depletion and sensitivity analysis in continuous energy
 - Extended modern, modular software design
- ### Expanded Integration
- Tools directly integrated with many projects



SCALE criticality validation: Verified, Archived Library of Inputs and Data (VALID)

- 611 configurations from International Criticality Safety Benchmark Evaluation Project (ICSBEP)
- 200 additional configurations, especially for ^{233}U systems



Sequence / Geometry	Experiment class	ICSBEP case numbers	Number of configurations
CSAS5 / KENO V.a	HEU-MET-FAST	15, 16, 17, 18, 19, 20, 21, 25, 30, 38, 40, 52, 65	19
	HEU-SOL-THERM	1, 13, 14, 16, 28, 29, 30	52
	IEU-MET-FAST	2, 3, 4, 5, 6, 7, 8, 9	8
	LEU-COMP-THERM	1, 2, 8, 10, 17, 42, 50, 78, 80	140
	LEU-SOL-THERM	2, 3, 4	19
	MIX-MET-FAST	5, 6	2
	MIX-COMP-THERM	1, 2, 4	21
	MIX-SOL-THERM	2, 7	10
	PU-MET-FAST	1, 2, 5, 6, 8, 10, 18, 22, 23, 24, 25, 26	12
	PU-SOL-THERM	1, 2, 3, 4, 5, 6, 7, 11, 20	81
	U233-COMP-THERM	1	3
	U233-MET-FAST	1, 2, 3, 4, 5, 6	10
	U233-SOL-INTER	1	29
	U233-SOL-MIXED	1, 2	8
	U233-SOL-THERM	1, 2, 3, 4, 5, 8, 9, 11, 12, 13, 15, 16, 17	140
CSAS6 / KENO-VI	HEU-MET-FAST	5, 8, 9, 10, 11, 13, 24, 80, 86, 92, 93, 94	27
	IEU-MET-FAST	19	2
	MIX-COMP-THERM	8	28

• Fissile materials

- High-enriched uranium (HEU),
- Intermediate-enriched uranium (IEU)
- Low-enriched uranium (LEU)
- Plutonium (Pu)
- Mixed uranium/plutonium oxides (MOX)
- Uranium-233 (U233)

• Fuel form

- Metal (MET),
- Fissile solution (SOL)
- Multi-material composition (e.g. fuel pins – COMP)

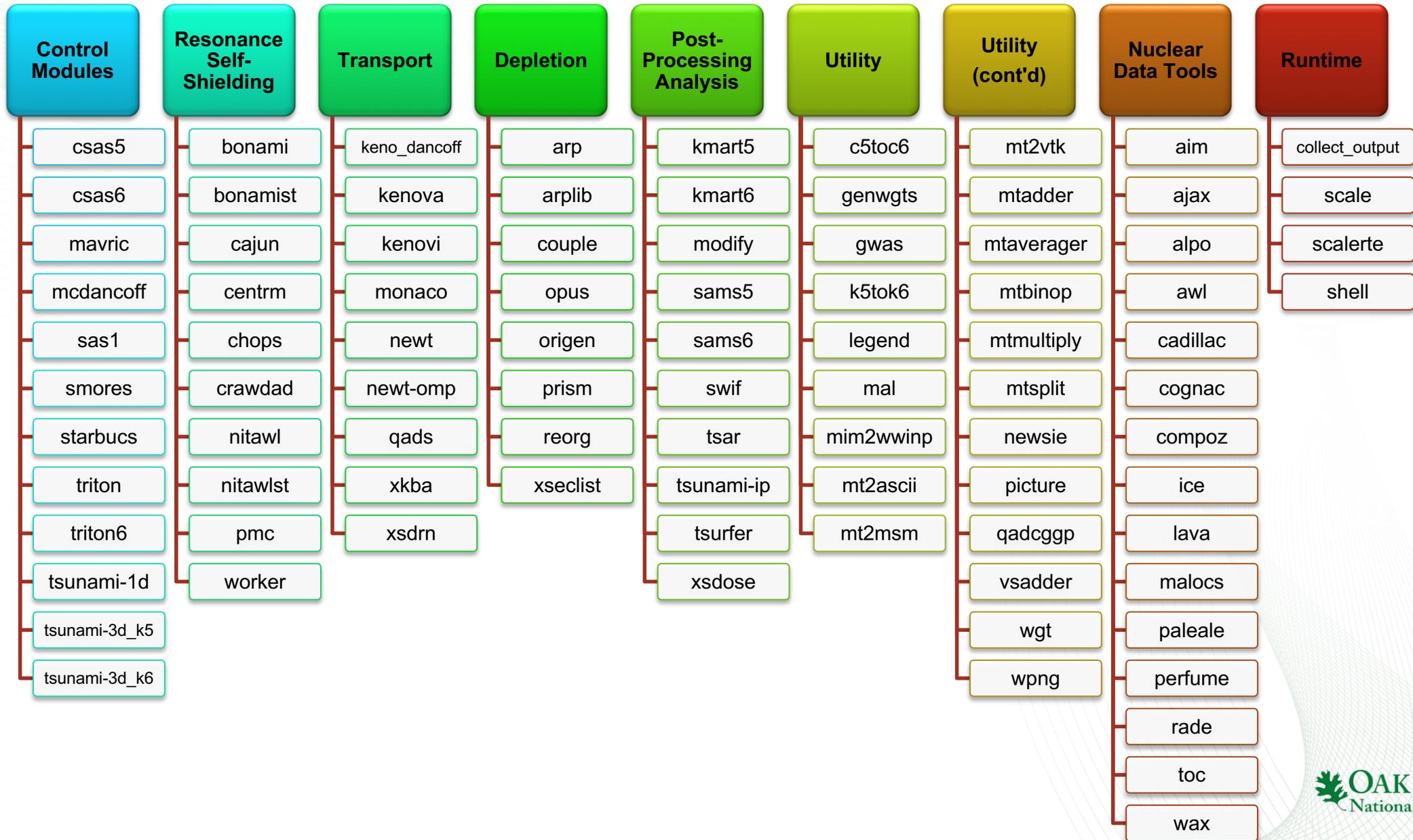
• Neutron spectra

- Fast
- Intermediate (INTER)
- Thermal
- Mixed

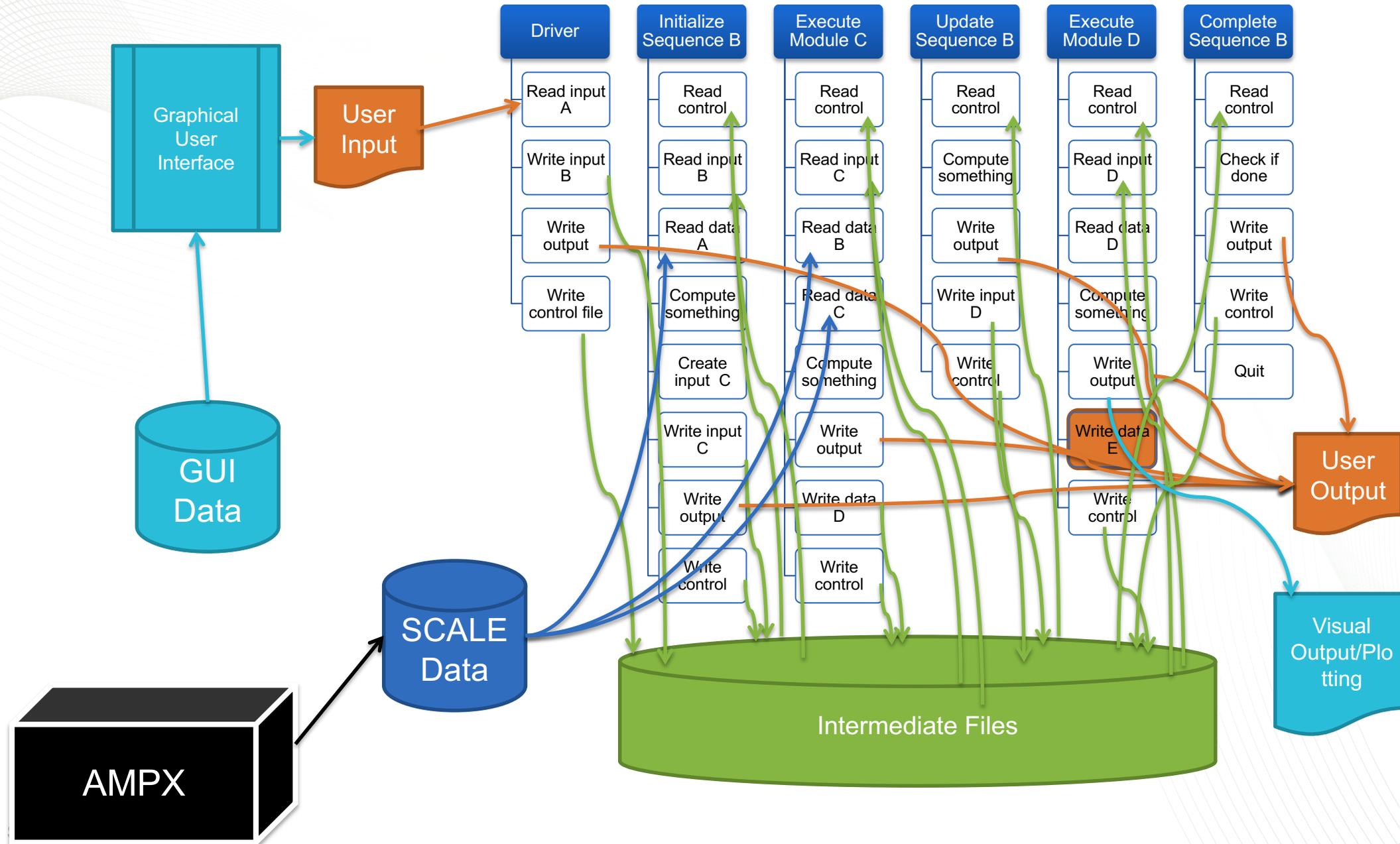


SCALE Modernization Plan:

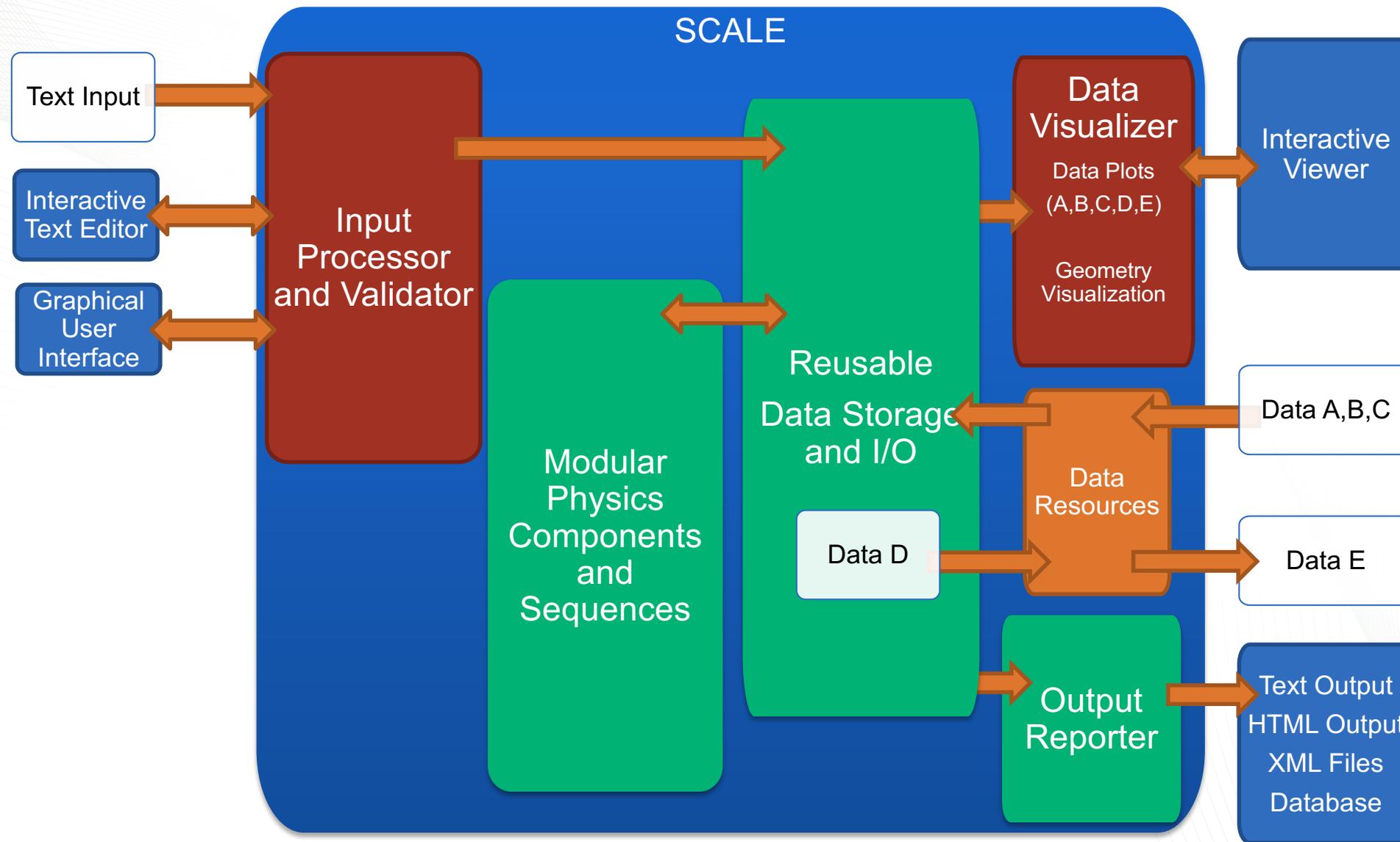
89 Independent Executable Modules in SCALE 6.1



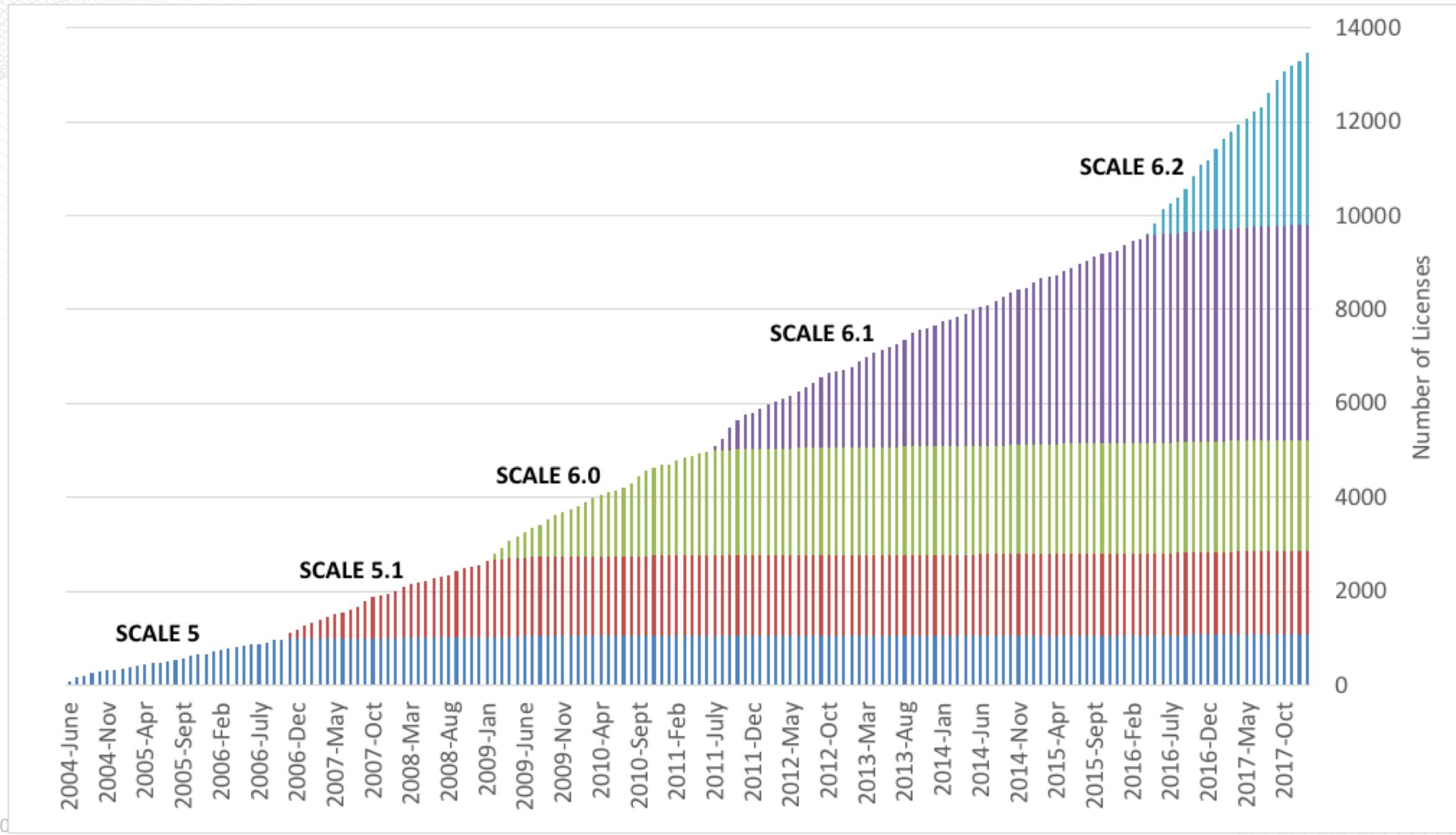
Hypothetical SCALE 6.1 Calculation



SCALE 7 Modernized Concept



SCALE licenses by version



Shift Monte Carlo code system

- Flexible, high-performance Monte Carlo radiation transport *framework*
- Shift is physics agnostic
 - SCALE CE physics
 - SCALE MG physics
- Shift is geometry agnostic
 - SCALE geometry
 - Exnihilo RTK geometry
 - MCNP geometry
 - DagMC-CUBIT CAD geometry



- Fixed-source and eigenvalue solvers
- Integrated with Denovo for hybrid methods
- Multiple parallel decompositions and concurrency models
- Shift is designed to scale from supercomputers to laptops

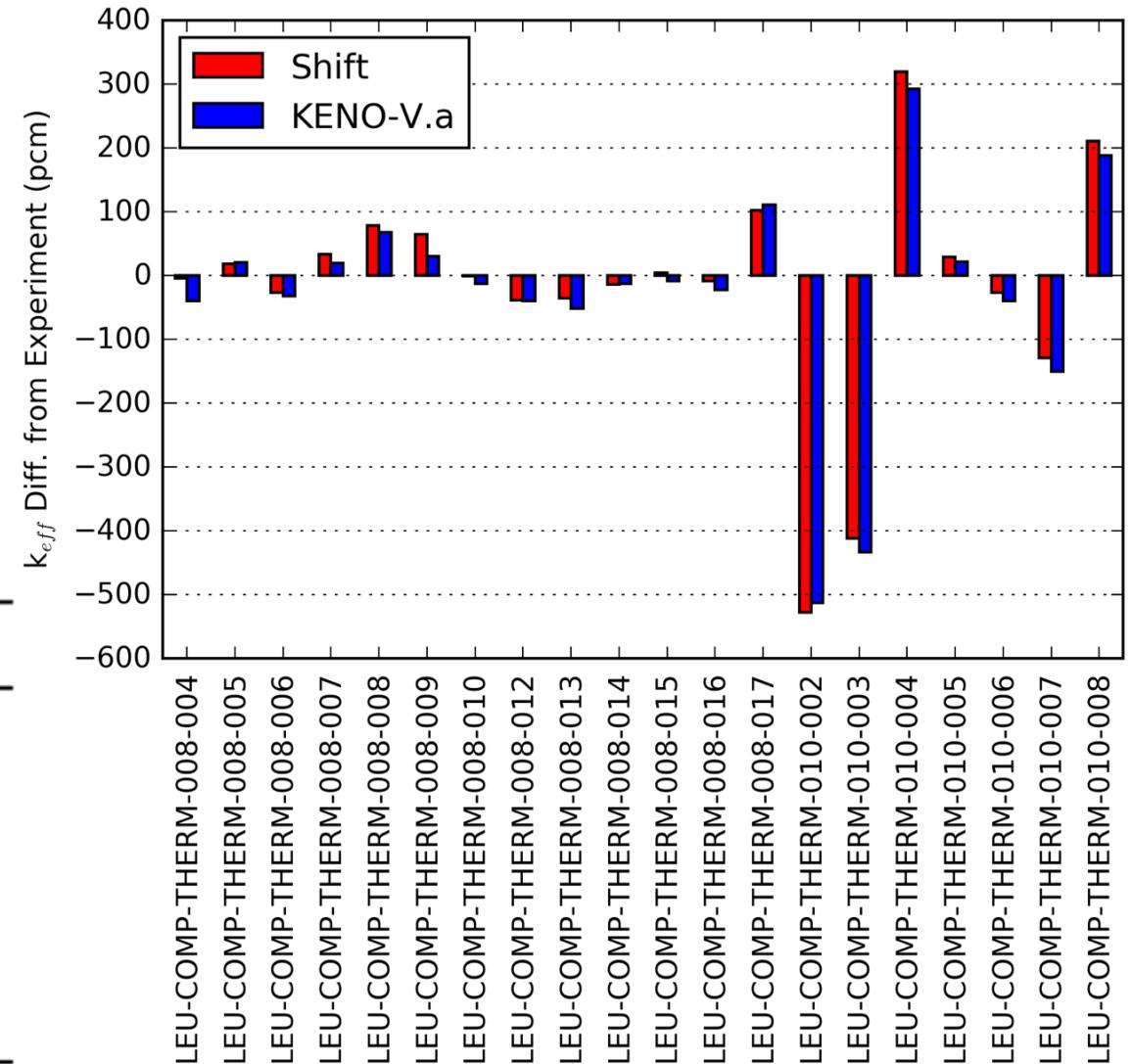
Validation of CSAS5-Shift

- VALID results for Shift correspond well with KENO V.a and KENO-VI results
- VALID calculations were run on a single processor, to compare computational time between KENO and Shift

Experiment type	Number of cases	Difference from KENO ^a (pcm)	Standard deviation ^b (pcm)
LEU-COMP-THERM	128	21	31
IEU-MET-FAST	11	16	160
PU-MET-FAST	10	-23	27
MIX-SOL-THERM	3	23	21
MIX-COMP-FAST	2	506	19
MIX-COMP-THERM	20	18	17
HEU-MET-FAST	22	-14	18
PU-SOL-THERM	81	6	20

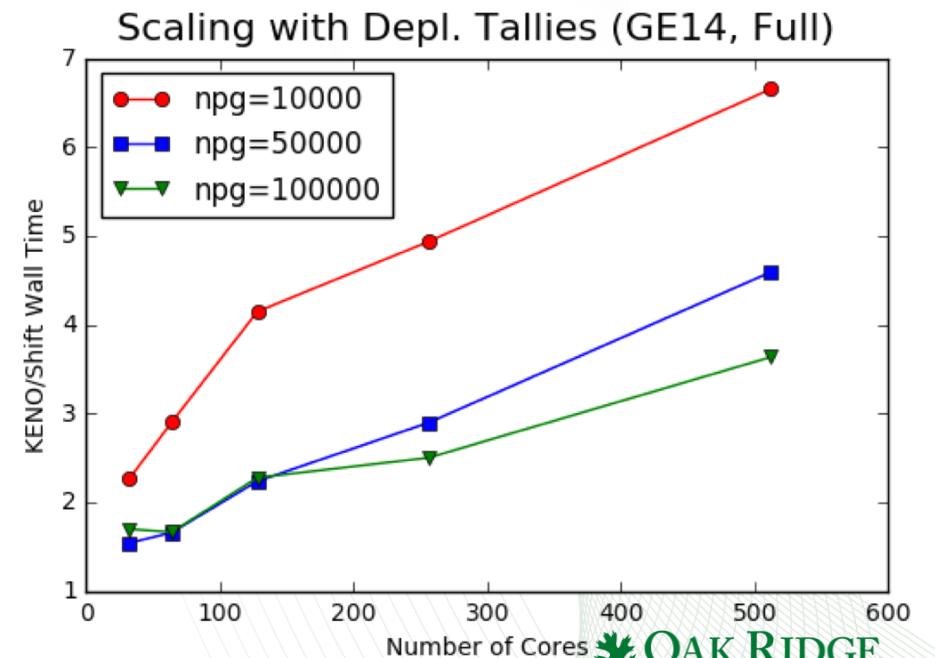
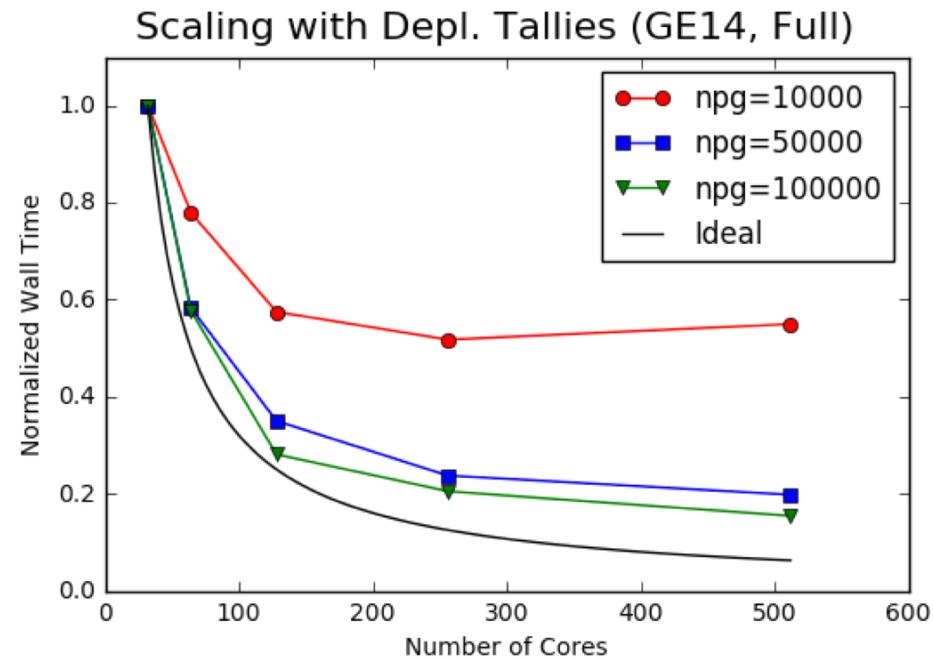
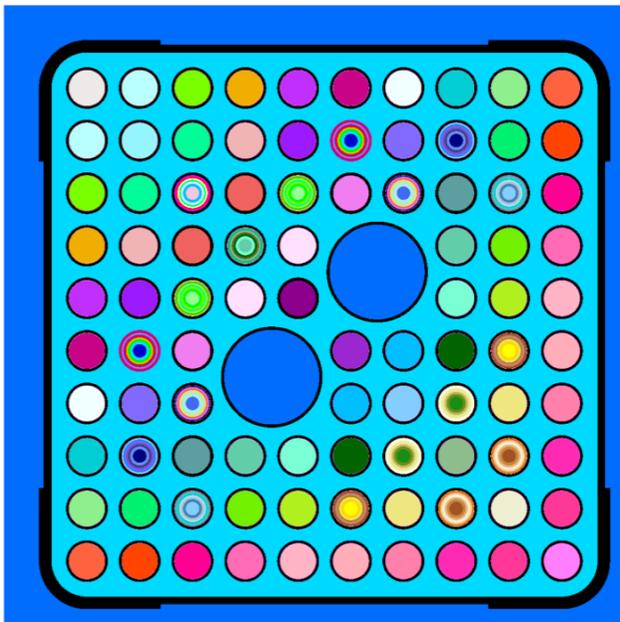
^a Computed as the average over all KENO and Shift simulations for an experiment set.

^b Computed as the standard deviation of the difference in k_{eff} between Shift and KENO.

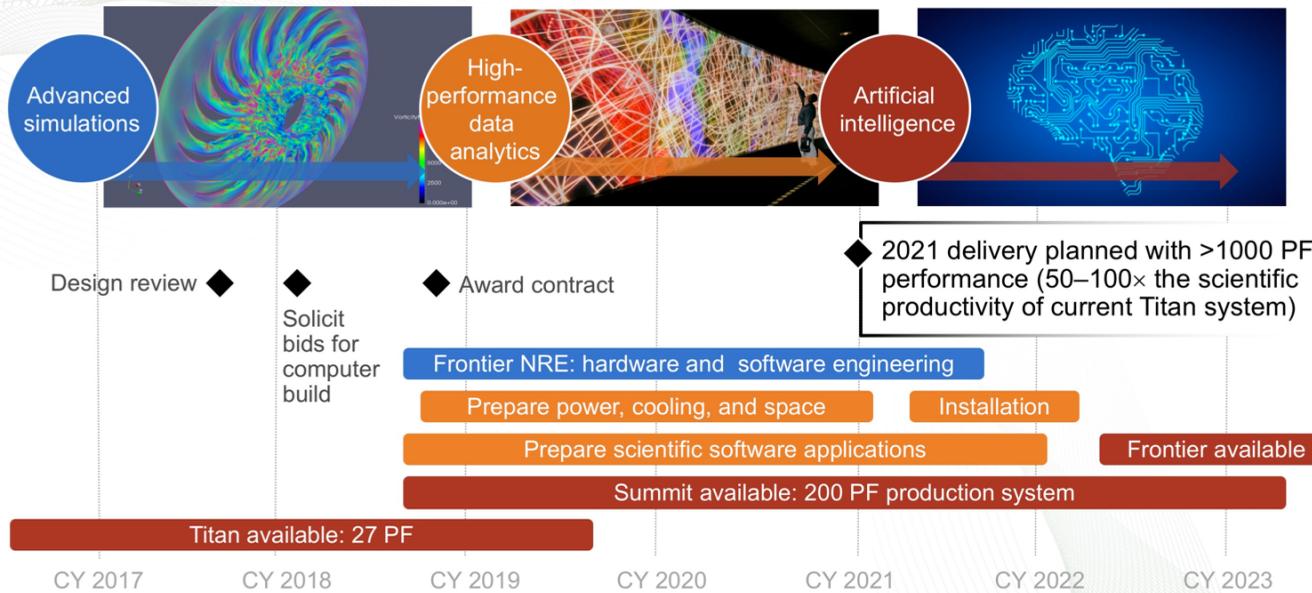


Shift parallel scaling compared to KENO

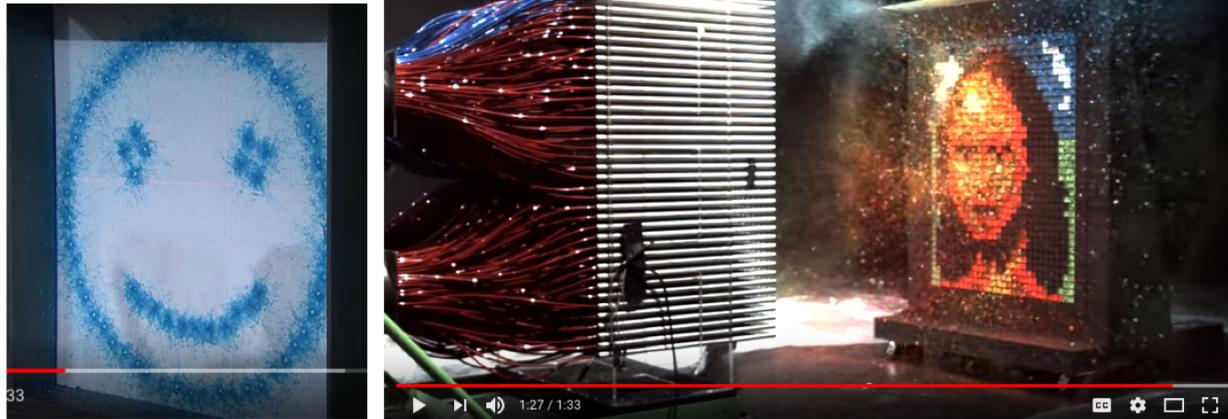
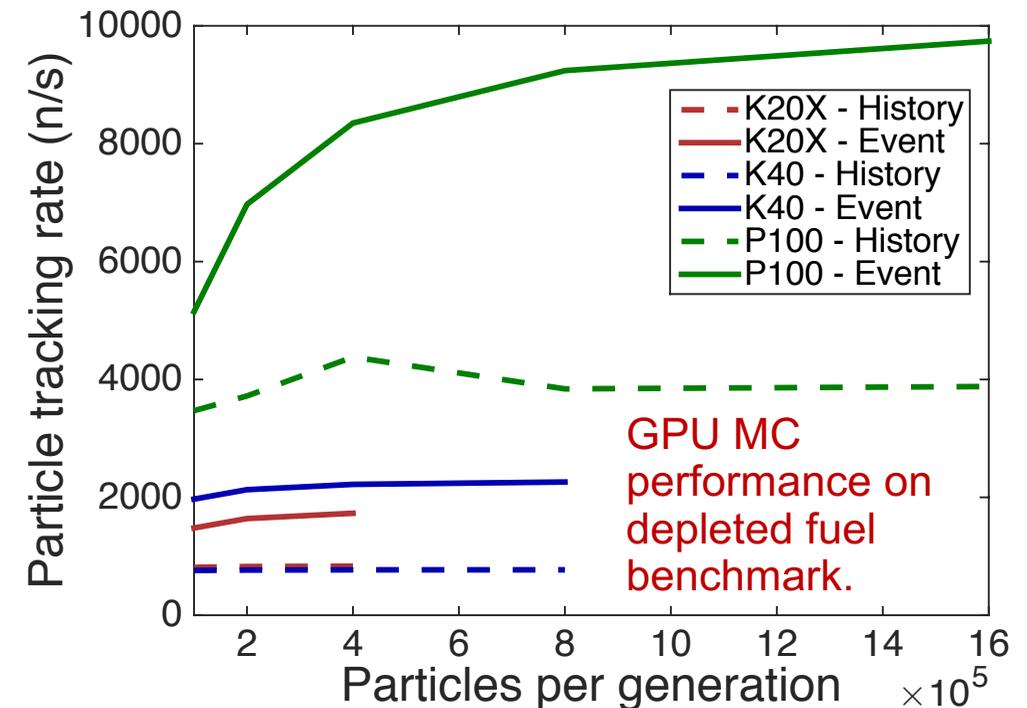
- **Test Case:** GE14 fuel assembly with depletion tallies
 - A number of identical simulations were run and the average time over the set simulations was used to estimate CPU time
- Shift is only slightly faster than KENO on a single node (1.5x – 2x), but much faster on many nodes (3x - 7x)
- Shift scales close to ideally up to hundreds of processors when using O(50k) particles per generation



Shift is being extended for operation on GPUs as part of the Exascale Computing Project

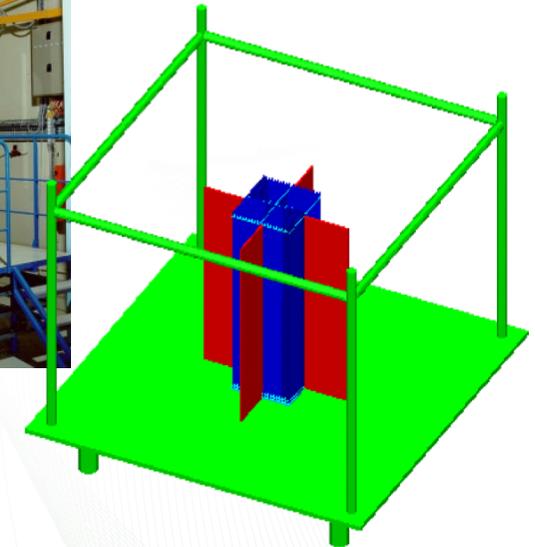


- Improved Monte Carlo particle tracking rate allows reduction in statistical errors
- Cost of tallies and data access is implicit in this measure
- Improved device performance yields better results – Algorithms are tracking hardware improvements



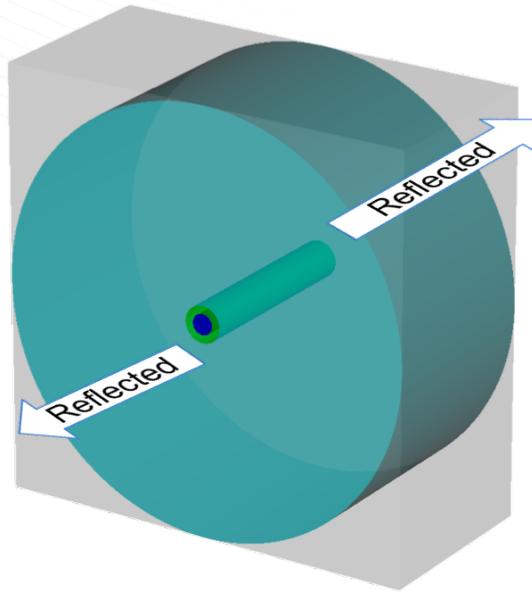
Shift/SCALE integration

- **Integrated in CSAS criticality sequence**
 - Eigenvalue mode for criticality safety
 - KENO V.a and KENO-VI geometry
 - Uses standard SCALE geometry, material, and control specifications
 - Validated with over 400 benchmark experiments
- **Integration in TRITON depletion sequence**
 - Currently in development
 - Flux-solver
 - Depletion
 - Multigroup cross section generation for nodal codes
 - Randomized geometry for TRISO and pebble bed
- **Integration in TSUNAMI sensitivity/uncertainty sequences**
 - Capability demonstrated
 - Eigenvalue and generalized perturbation theory sensitivity coefficients with CE physics
- **Integration in MAVRIC shielding sequence**
 - Fixed-source shielding problems using hybrid methods, especially for large facility and site modeling
 - Currently in development

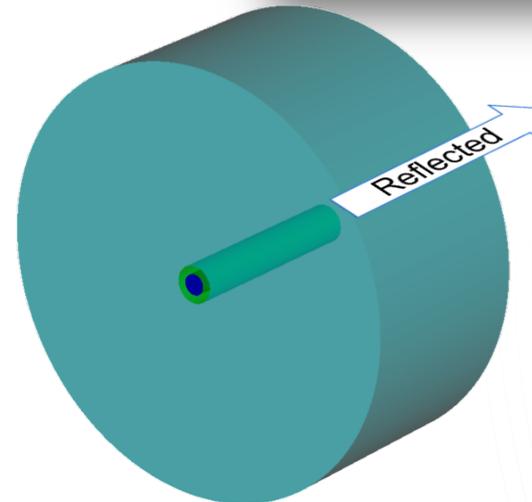


SCALE User Notice – March 2018

- A check that users enter a required cuboidal outer boundary if using non-vacuum boundary conditions was disabled for SCALE 6.1–6.2.2
- Check enabled again for SCALE 6.2.3



Correct
Cuboid boundary
 $k_{\text{eff}} = 1.03599 \pm 0.00063$



Incorrect
No-cuboidal boundary
 $k_{\text{eff}} = 1.01098 \pm 0.00070$

SCALE User Notice

March 8, 2018

The KENO V.a Monte Carlo code in SCALE 6.1–6.2.2 does not include an input check to ensure compliance with the requirement that albedo boundary conditions other than vacuum (e.g., mirror, periodic, white) are only applied to cuboidal outer shapes. Users who do not follow this requirement per the user documentation may generate non-conservative k_{eff} results without warning.

Per the requirements of the *Quality Assurance Plan for the SCALE Code System* [1] and specifically the *SCALE Procedure for Discrepancy Reports* [2], this issue is being categorized as a *Significant Software Error* and is reported in this User Notice.

Summary

In all versions of SCALE, the Monte Carlo code KENO V.a only implements the use of non-vacuum albedo boundary conditions (e.g., mirror, periodic, white) when the outermost geometry region of the model is a cuboidal region. This limitation is noted in the user documentation in the section on *Albedo data*, where it is stated that “Albedo boundary conditions are applied only to the outermost region of a problem. In KENO V.a this geometry region must be a rectangular parallelepiped”[3][4].

I have to say I am very impressed by the SCALE team's response here. This is a code system that is clearly professionally run and most importantly communicative with its users.

– Don Algama – U.S. Nuclear Regulator Commission

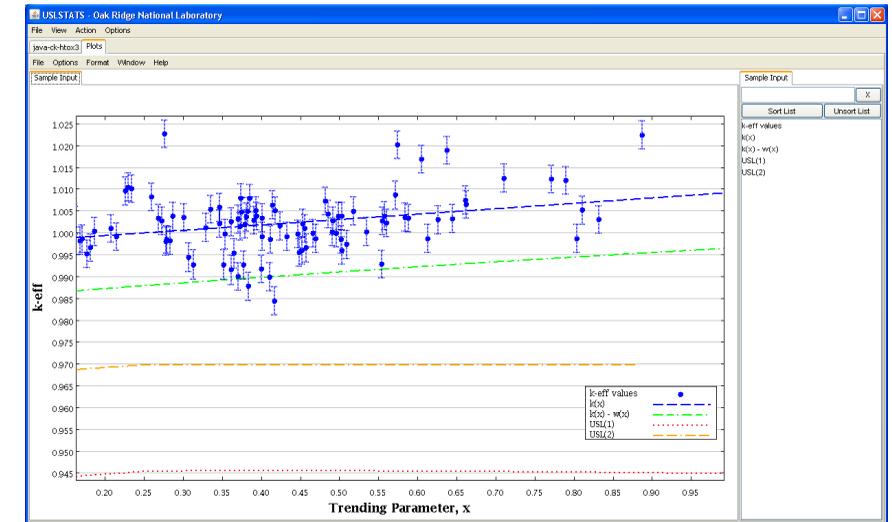
Modernization of USLSTATS

Statistical package for determining upper subcritical limits using traditional or S/U-based parameters

SCALE 6.2:

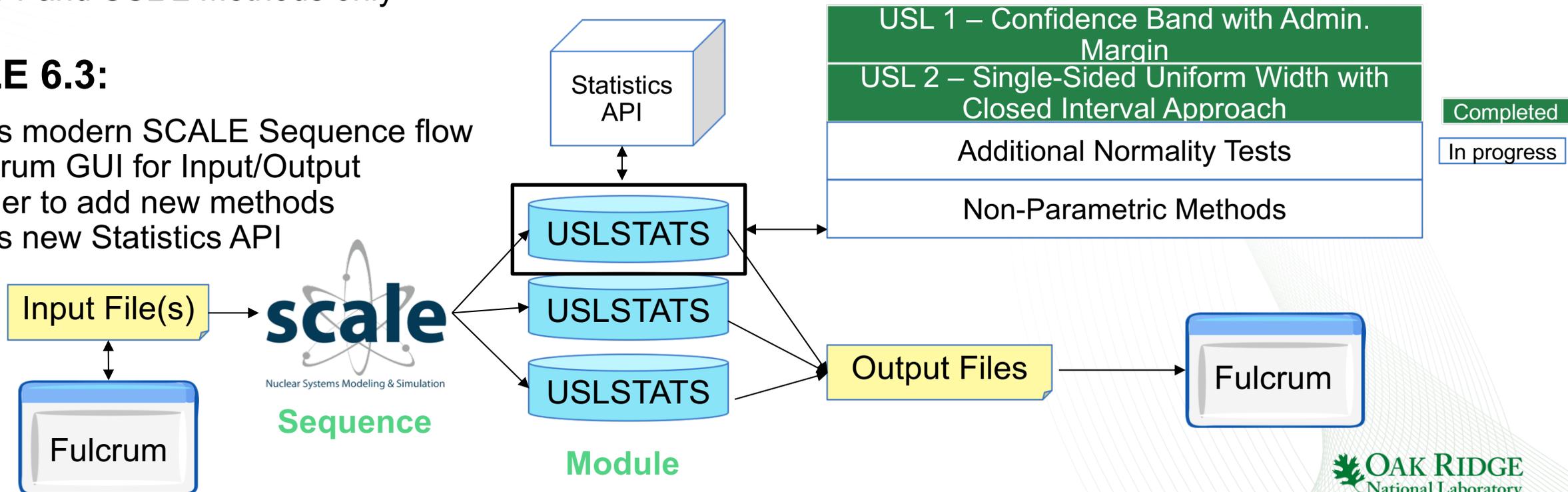


- Java code not routinely tested with rest of SCALE
- USL 1 and USL 2 Methods only



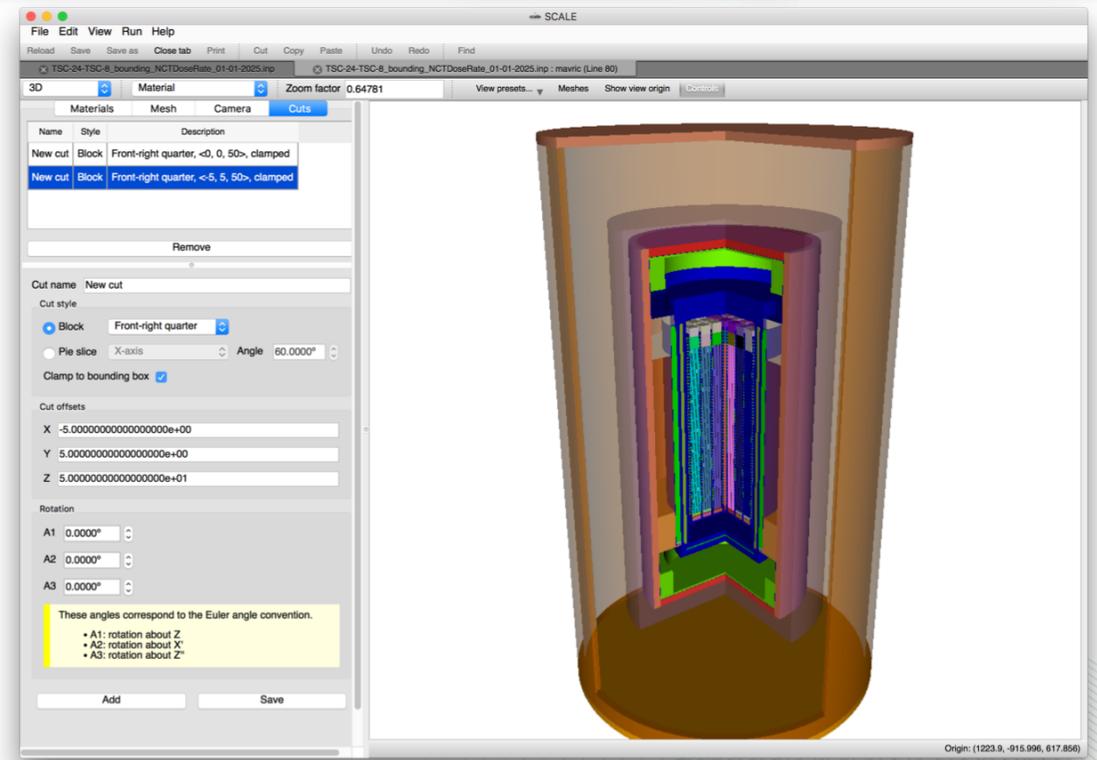
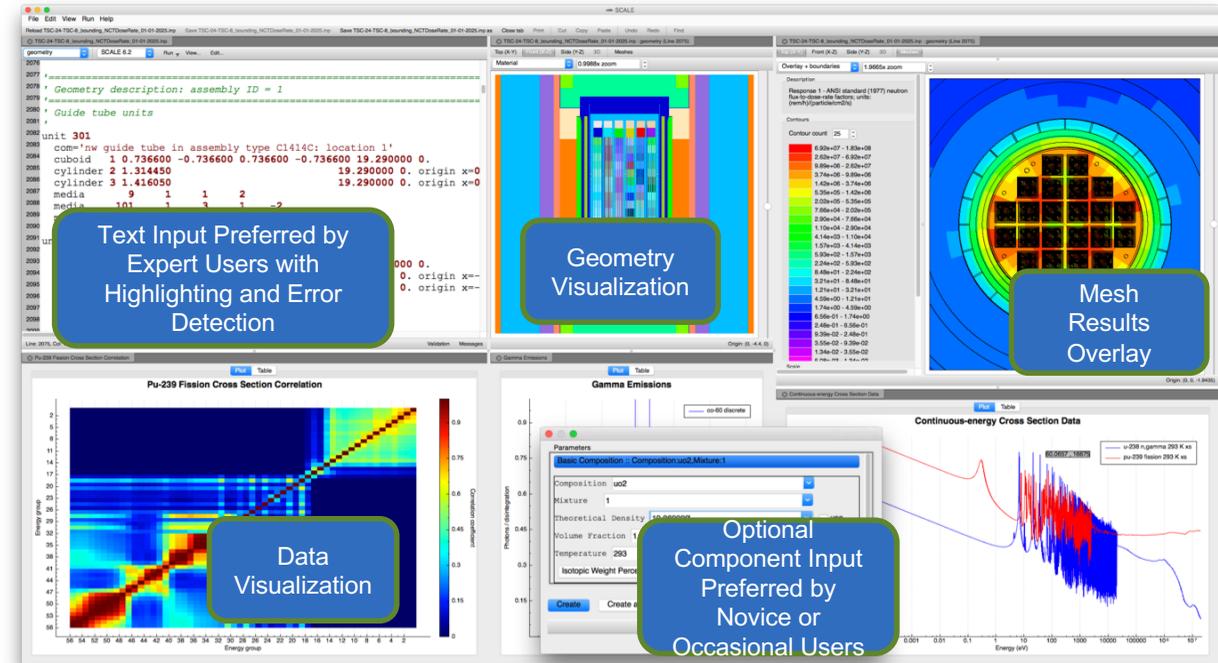
SCALE 6.3:

- Uses modern SCALE Sequence flow
- Fulcrum GUI for Input/Output
- Easier to add new methods
- Uses new Statistics API



Fulcrum: SCALE's integrated user interface

- Input generation and checking
- Geometry and nuclear data visualization
- Output review and visualization
- New 3D visualization for KENO V.a and KENO-VI
 - Multiple cuts with “undo”
 - Transparency
 - Rotation
 - Hide/Show materials
- Pending development:
 - AMPX integration (currently uses ExSITE)
 - Coloring for computed values instead of just materials
 - Mesh results overlay in 3D
 - Expanded use of input generation from dialog boxes, especially for new users



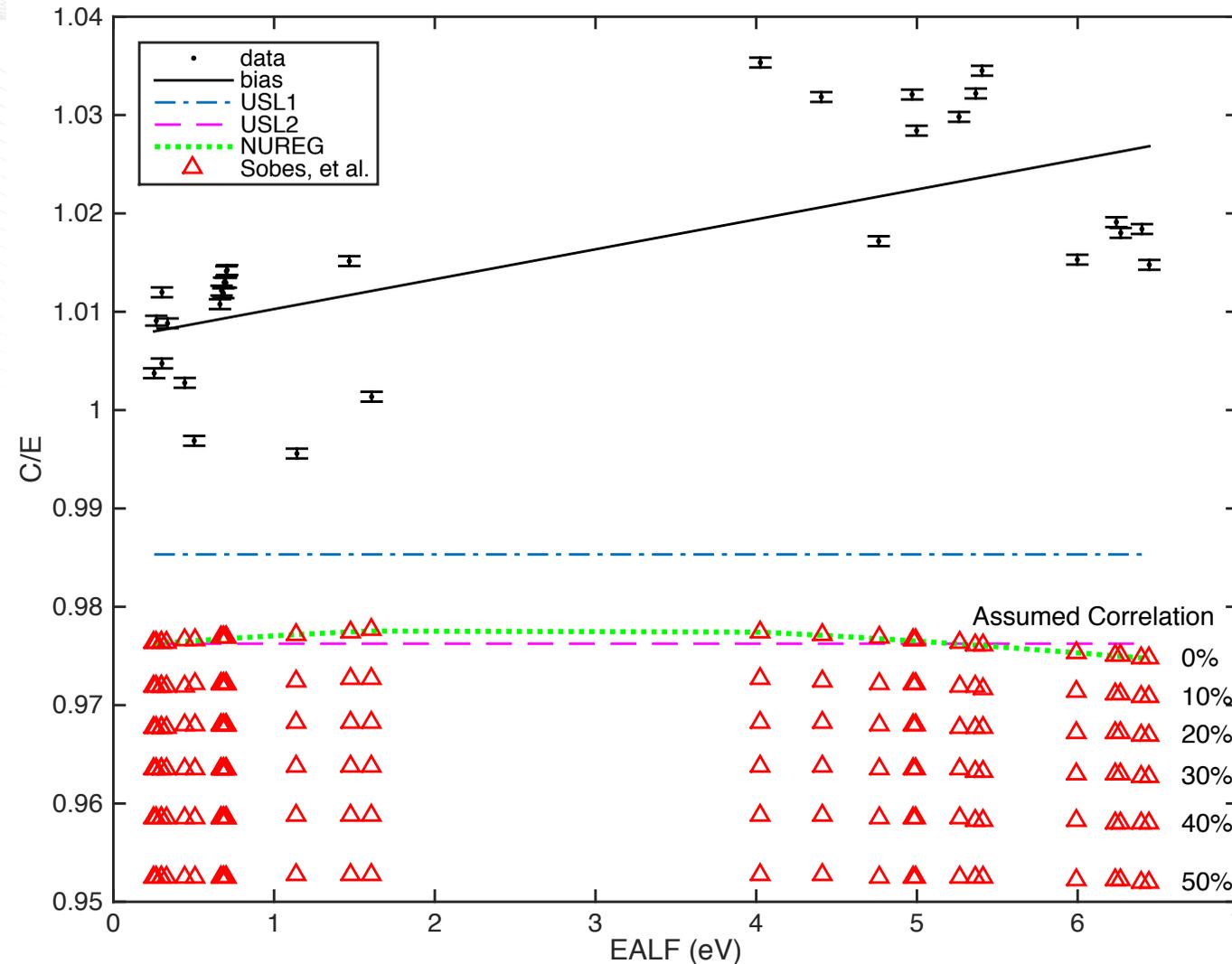
Uncertainty Analysis for Criticality Safety Assessment (UACSA)

- OECD/NEA expert group under Working Party on Nuclear Criticality Safety
- Nearly 40 participants
- Phase IV Benchmark on *Role of Integral Experiment Covariance Data for Criticality Safety Validation*
- Phase V Benchmark *Blind Benchmark on MOX Wet Powders*



Phase IV Benchmark

Role of Integral Experiment Covariance Data for Criticality Safety Validation



- Using data from a previous transportation package criticality safety assessment, the inclusion of experimental correlations impacts the USL by as much as **3% $\Delta k/k$**

V. Sobes, B. T. Rearden, D. E. Mueller, W. J. Marshall, J. M. Scaglione, and M. E. Dunn, "Upper Subcritical Calculations Based on Correlated Data," ICNC 2015 – International Conference on Nuclear Criticality Safety, Charlotte, NC, September 13–17, 2015.

WPNCS/UACSA results

Fully correlated

	7-1	7-2	7-3	39-1	39-2	39-3	39-4	39-5	39-6	39-7	39-8	39-9	39-10	39-11	39-12	39-13	39-14	39-15	39-16	39-17
7-1	1.000	0.933	0.391	0.978	0.975	0.974	0.974	0.956	0.957	0.974	0.971	0.978	0.969	0.977	0.972	0.980	0.979	0.973	0.977	0.978
7-2	0.933	1.000	0.557	0.923	0.920	0.925	0.930	0.925	0.929	0.933	0.920	0.936	0.940	0.925	0.924	0.928	0.933	0.928	0.937	0.931
7-3	0.391	0.557	1.000	0.405	0.390	0.409	0.417	0.459	0.463	0.415	0.389	0.434	0.451	0.384	0.406	0.405	0.382	0.399	0.418	0.420
39-1	0.978	0.923	0.405	1.000	0.978	0.970	0.973	0.957	0.958	0.976	0.972	0.970	0.973	0.979	0.976	0.976	0.981	0.977	0.972	0.977
39-2	0.975	0.920	0.390	0.978	1.000	0.972	0.970	0.953	0.954	0.975	0.967	0.968	0.963	0.974	0.974	0.976	0.977	0.970	0.972	0.977
39-3	0.974	0.925	0.409	0.970	0.972	1.000	0.967	0.945	0.954	0.971	0.963	0.971	0.966	0.974	0.969	0.974	0.971	0.967	0.972	0.970
39-4	0.974	0.930	0.417	0.973	0.970	0.967	1.000	0.956	0.954	0.971	0.965	0.968	0.965	0.972	0.971	0.973	0.974	0.968	0.973	0.978
39-5	0.956	0.925	0.459	0.957	0.953	0.945	0.956	1.000	0.946	0.958	0.944	0.955	0.955	0.953	0.949	0.952	0.952	0.954	0.951	0.958
39-6	0.957	0.929	0.463	0.958	0.954	0.954	0.954	0.946	1.000	0.956	0.953	0.960	0.961	0.955	0.954	0.963	0.955	0.957	0.958	0.960
39-7	0.974	0.933	0.415	0.976	0.971	0.971	0.971	0.958	0.956	1.000	0.973	0.974	0.970	0.979	0.978	0.974	0.979	0.974	0.979	0.978
39-8	0.971	0.920	0.389	0.972	0.967	0.963	0.965	0.944	0.953	0.973	1.000	0.964	0.970	0.973	0.966	0.970	0.973	0.964	0.964	0.966
39-9	0.978	0.936	0.434	0.970	0.968	0.971	0.968	0.955	0.960	0.974	0.964	1.000	0.967	0.976	0.968	0.976	0.976	0.969	0.975	0.974
39-10	0.969	0.940	0.451	0.973	0.963	0.966	0.965	0.955	0.961	0.970	0.970	0.967	1.000	0.964	0.968	0.969	0.966	0.964	0.968	0.970
39-11	0.977	0.925	0.384	0.979	0.974	0.974	0.972	0.953	0.955	0.979	0.973	0.976	0.964	1.000	0.973	0.980	0.979	0.977	0.977	0.977
39-12	0.972	0.924	0.406	0.976	0.974	0.969	0.971	0.949	0.954	0.978	0.966	0.968	0.968	0.973	1.000	0.978	0.976	0.968	0.972	0.976
39-13	0.980	0.928	0.405	0.976	0.976	0.974	0.973	0.952	0.963	0.974	0.970	0.976	0.969	0.980	0.978	1.000	0.977	0.979	0.976	0.976
39-14	0.979	0.933	0.382	0.981	0.977	0.971	0.974	0.952	0.955	0.979	0.973	0.976	0.966	0.979	0.976	0.977	1.000	0.976	0.977	0.979
39-15	0.973	0.928	0.399	0.977	0.970	0.967	0.968	0.954	0.957	0.974	0.964	0.969	0.964	0.977	0.968	0.979	0.976	1.000	0.970	0.973
39-16	0.977	0.937	0.418	0.972	0.972	0.972	0.973	0.951	0.958	0.979	0.964	0.975	0.968	0.977	0.972	0.976	0.977	0.970	1.000	0.976
39-17	0.978	0.931	0.420	0.977	0.977	0.970	0.978	0.958	0.960	0.978	0.966	0.974	0.970	0.977	0.976	0.976	0.979	0.973	0.976	1.000

Pitch sampled: all pitches are the same and are the same for all cases

Coefficients range from 0.96 to 0.98
(For cases with the same pitch)

Independent

	7-1	7-2	7-3	39-1	39-2	39-3	39-4	39-5	39-6	39-7	39-8	39-9	39-10	39-11	39-12	39-13	39-14	39-15	39-16	39-17
7-1	1.000	0.034	0.023	0.012	0.005	-0.040	0.069	-0.009	0.071	0.067	0.082	0.088	0.049	0.044	0.042	0.063	0.088	0.139	-0.021	0.082
7-2	0.034	1.000	0.074	-0.045	0.020	0.040	0.181	0.086	0.065	0.041	-0.028	-0.034	0.009	-0.030	0.018	0.047	-0.041	0.023	0.061	-0.028
7-3	0.023	0.074	1.000	0.118	0.063	0.094	0.061	0.086	0.201	0.079	0.100	0.134	0.047	0.091	0.012	0.125	0.050	0.117	0.172	0.055
39-1	0.012	-0.045	0.118	1.000	0.121	0.138	0.076	0.071	0.124	0.034	0.100	0.085	0.135	0.023	0.037	0.037	0.087	0.083	0.115	0.149
39-2	0.005	0.020	0.063	0.121	1.000	0.034	0.075	0.037	0.130	0.041	0.055	0.049	0.009	0.025	0.095	0.100	-0.050	0.124	-0.003	0.115
39-3	-0.040	0.040	0.094	0.138	0.034	1.000	0.079	0.077	0.044	0.007	0.048	-0.064	0.145	0.076	0.061	0.090	0.067	0.059	0.088	0.116
39-4	0.069	0.181	0.061	0.076	0.075	0.079	1.000	-0.051	0.090	-0.012	-0.017	0.036	0.026	-0.021	0.034	0.088	0.042	-0.004	0.025	-0.018
39-5	-0.009	0.086	0.086	0.071	0.037	0.077	-0.051	1.000	0.138	0.081	0.043	0.140	0.112	0.059	0.085	0.131	0.184	0.001	0.161	0.093
39-6	0.071	0.065	0.201	0.124	0.130	0.044	0.090	0.138	1.000	0.103	-0.014	0.035	0.149	0.051	0.062	0.116	0.013	0.074	0.153	0.127
39-7	0.067	0.041	0.079	0.034	0.041	0.007	-0.012	0.081	0.103	1.000	0.131	-0.007	0.004	0.024	-0.003	0.111	0.053	0.081	0.173	0.035
39-8	0.082	-0.028	0.100	0.100	0.055	0.048	-0.017	0.043	-0.014	0.131	1.000	-0.067	0.047	-0.016	0.063	0.004	0.030	0.013	0.050	0.070
39-9	0.088	-0.034	0.134	0.085	0.049	-0.064	0.036	0.140	0.035	0.007	-0.067	1.000	0.082	0.041	0.070	0.000	0.046	-0.081	-0.009	0.077
39-10	0.049	0.009	0.047	0.135	0.009	0.145	0.026	0.112	0.149	0.004	0.047	0.082	1.000	0.080	0.069	-0.004	0.041	0.115	0.119	0.047
39-11	0.044	-0.030	0.091	0.023	0.025	0.076	-0.021	0.059	0.051	-0.024	-0.016	0.041	0.080	1.000	0.115	0.022	-0.087	-0.048	0.112	0.046
39-12	0.042	0.018	0.012	0.037	0.095	0.061	0.034	0.085	0.062	-0.003	0.063	0.070	0.069	0.115	1.000	0.132	0.112	0.006	0.065	0.069
39-13	0.063	0.047	0.125	0.037	0.100	0.090	0.088	0.131	0.116	0.111	0.004	0.000	-0.004	0.022	0.132	1.000	0.184	0.206	0.232	0.138
39-14	0.088	-0.041	0.050	0.087	-0.050	0.067	0.042	0.184	0.013	0.053	0.030	0.046	0.041	-0.087	0.112	0.184	1.000	0.148	0.051	0.204
39-15	0.139	0.023	0.117	0.083	0.124	0.059	-0.004	0.001	0.074	0.081	0.013	-0.081	0.115	-0.048	0.006	0.206	0.148	1.000	0.090	0.037
39-16	-0.021	0.061	0.172	0.115	-0.003	0.088	0.025	0.161	0.153	0.173	0.050	-0.009	0.119	0.112	0.065	0.232	0.051	0.090	1.000	-0.023
39-17	0.082	-0.028	0.055	0.149	0.115	0.116	-0.018	0.093	0.127	0.035	0.070	0.077	0.047	0.046	0.069	0.138	0.204	0.037	-0.023	1.000

All fuel rod positions are sampled independently and differently in each case

Coefficients range from ~0 to ~0.23

Fuel rod position modeling makes a difference!

W. J. Marshall and B. T. Rearden, "Determination of Critical Experiment Correlations for Experiments Involving Arrays of Low-Enriched Fuel Rods," *Proc. of ANS NCSD 2017 - Criticality safety - pushing the boundaries by modernizing and integrating data, methods, and regulations*, Carlsbad, NM, September 10–15, 2017.

Phase V Benchmark

Blind Benchmark on MOX Wet Powders

- Challenging criticality safety validation with few applicable benchmark
- Advanced validation methods such as TSURFER and Whisper are required

BFS Cases

HEU-MET-FAST

HEU-SOL-THERM

IEU-MET-FAST

LEU-COMP-THERM

LEU-MET-THERM

LEU-SOL-THERM

MIX-COMP-THERM

MIX-COMP-FAST

Case	Comp 1	Comp 2	Comp 3	Comp 4	Comp 5	Comp 6	Comp 7	Comp 8	Comp 9	Comp 10	Comp 11	Comp 12	Comp 13	Comp 14	Comp 15	Comp 16	Comp 17	Comp 18	Comp 19	Comp 20	Comp 21	Comp 22	Comp 23	Comp 24	Comp 25
MIX-COMP-FAST-001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001

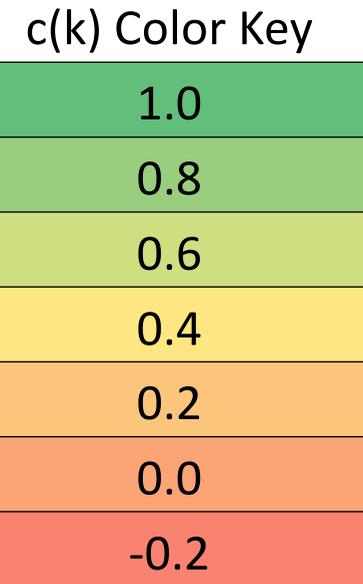
MIX-MISC-THERM

MIX-SOL-THERM

PU-COMP-MIXED

PU-MET-FAST

PU-SOL-THERM



Phase V Benchmark

Blind Benchmark on MOX Wet Powders

- USLs vary from 0.74 to 0.99 based on selected benchmarks and validation approach

	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6	Case 7	Case 8	Case 9	Case 10	Case 11	Case 12	Case 13	Case 14	Case 15
USLSTATS Trending with PU-COMP-MIXED Experiments															
$c(k) > 0.2$	0.9861	0.9772	0.9845	0.9856	0.9765	0.9912	0.9886	0.9818	0.9882	0.9860	0.9819	0.9886	0.9861	0.9762	0.9818
$c(k) > 0.55$	0.9754	0.9262	0.9883	0.9758	0.9462	0.9856	0.9832	0.9461	0.9895	0.9748	0.9641	0.9825	0.9754	0.9039	0.9775
USLSTATS Trending without PU-COMP-MIXED Experiments															
$c(k) > 0.2$	0.9861	0.9772	0.9845	0.9856	0.9765	0.9912	0.9886	0.9818	0.9882	0.9860	0.9819	0.9886	0.9861	0.9762	0.9818
$c(k) > 0.55$	0.9088	0.9461	0.9883	0.7751	0.9703	0.9856	0.9794	0.9681	0.9898	0.9436	0.9420	0.9825	0.7425	0.9418	0.9775
Whisper Methodology															
$c(k) > 0.2$	0.9657	0.9645	0.9627	0.9654	0.9646	0.9773	0.9668	0.9651	0.9663	0.9662	0.9649	0.9740	0.9652	0.9642	0.9611
$c(k) > 0.55$	0.9856	0.9665	0.9909	0.9881	0.9693	0.9843	0.9706	0.9659	0.9719	0.9832	0.9671	0.9843	0.9878	0.9663	0.9924
TSURFER Data Assimilation															
$USL_{TSURFER}$	0.9924	0.9935	0.9889	0.9921	0.9928	0.9871	0.9946	0.9958	0.9950	0.9930	0.9936	0.9896	0.9916	0.9926	0.9885

New ENDF/B-VIII.0 disclaimer

- Added to ENDF repository by head of National Nuclear Data Center after issues were raised at November 2017 CSEWG meeting

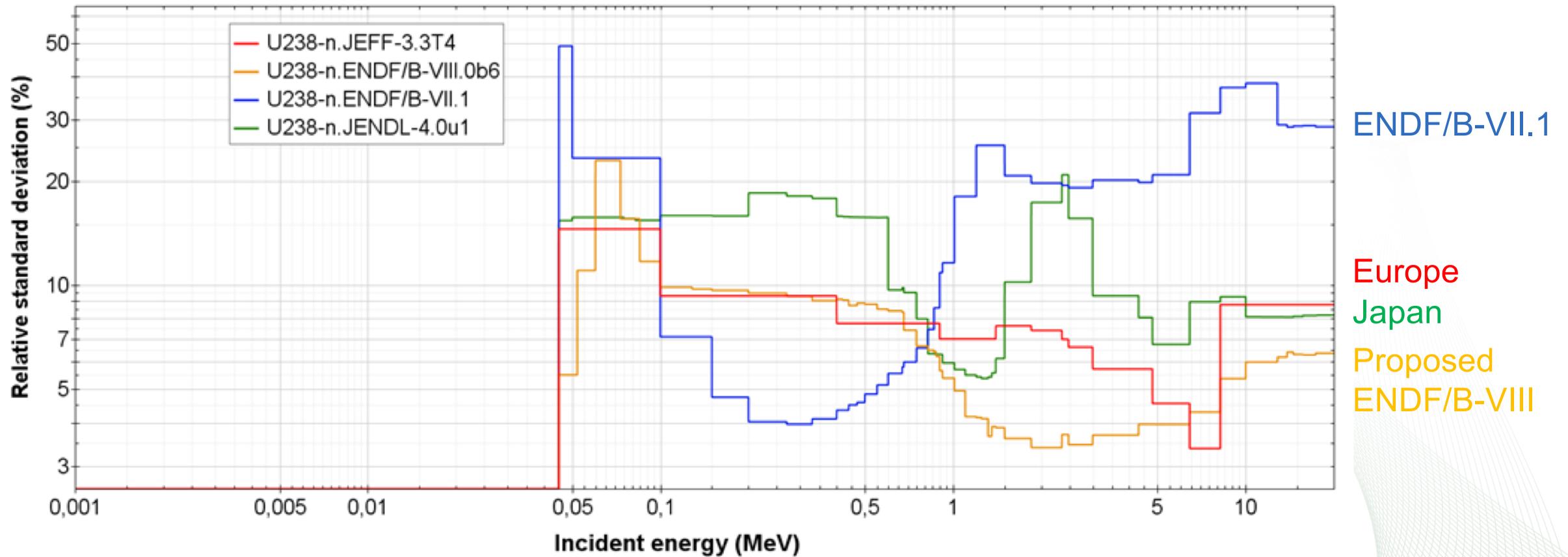
```
=====  
Readme for ENDF/B-VIII.0  
=====
```

Comments about the covariance in current ENDF evaluations

1. The covariance data in the ENDF evaluations represents uncertainties and correlations in differential data.
2. **The use of this covariance to calculate uncertainties for integral quantities such as K_{eff} will usually result in an overestimate of the uncertainty.**
3. The recommended methodology to overcome this problem is to adjust the covariance to add information from set of integral data that represents the physics of the system for which the adjusted covariance will be used.
4. More information on this topic: <https://www.oecd-nea.org/science/wpec/sg33/>
5. CSEWG is currently studying the best covariance representation for future releases.

^{238}U inelastic scattering cross section uncertainty differences between international libraries

Incident neutron data // U238 MAT9237 / MAT9237 / MT4= (n,n') / MT=4
: (z,n') / Covariances data (BOXER) Relative standard deviation



External Communication

- SCALE Website (scale.ornl.gov)
 - Publications/Training
 - Validation and benchmark reports
 - Downloads
- SCALE Newsletter
- SCALE Annual Report
- SCALE Users Group forum
- On-demand assistance
 - scalehelp@ornl.gov
- Facebook page
 - facebook.com/scale.codes

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SCALE training courses are routinely provided to the user community at ORNL and NEA, regulatory training is provided twice annually to NRC, and application-specific training provided at user facilities



- FY17 statistics:
- 10 one-week courses
- 4 conference tutorials
- 150 participants from 15 nations



SCALE Users' Group Workshop 2017



- The first ever SCALE Users' Group Workshop was held at ORNL, September 26-28, 2017
 - attended by 117 participants from academia, industry, research institutions, and government agencies
 - provided an interactive forum for discussions between SCALE end users and developers



Save the date: August 27–29, 2018
Application-specific technical tracks
Latest capabilities in SCALE 6.3
SCALE Help *Live!*